
Senior Petroleum Engineering Design

Recommendations for Developing a Barnett Gas Field Fort Worth Basin, Texas

Group 2

Jason Zhang

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Outline

- Motivation and Objective
- Study Area
- Workflow
- Rock Quality/Petrophysical Evaluation → Geological Modelling
- Completion Quality Evaluation → Hydraulic Fracture Modelling
- Field Evaluation → P_{50} Well Determination
- Operation Quality Evaluation → DCA, RTA
- Well Spacing Optimization
- Economic Viability of Development
- Conclusions and Recommendations
- Acknowledgements



Motivation and Objective

Motivation: *Operation “Stealthy Paws”*

- *Phase 1: Locate the package*
- *Phase 2: The Stakeout*
- *Phase 3: Steal Kalantari’s dog*
- *Phase 4: Pet it.*
- *Phase 5: Return*

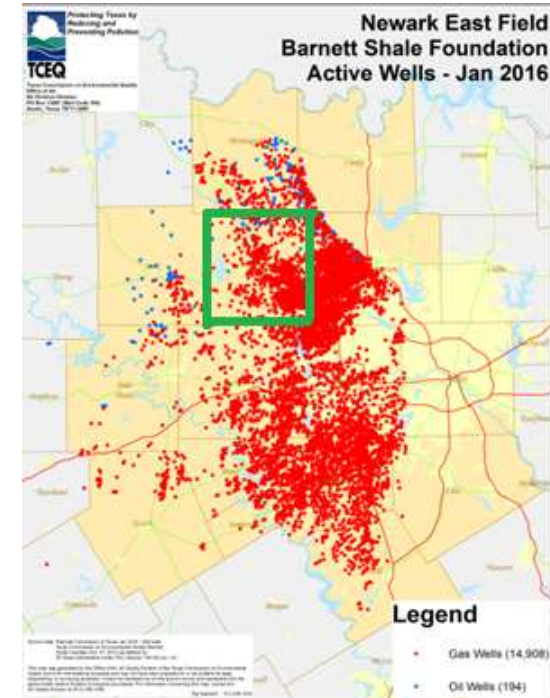
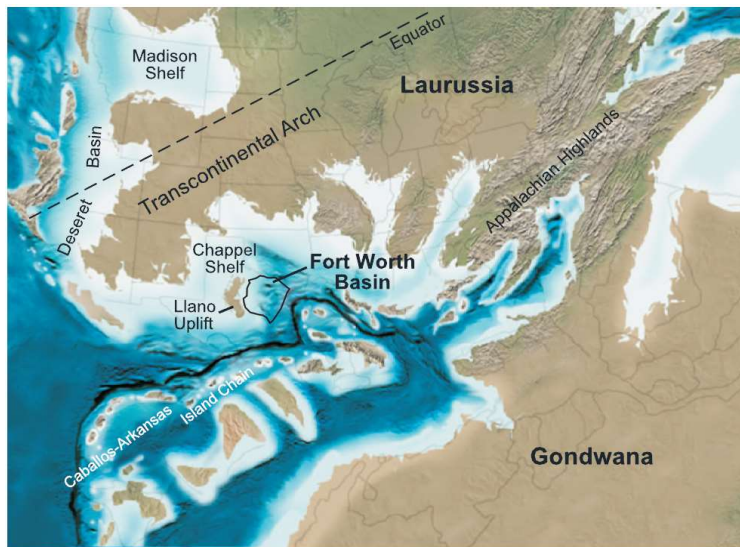


The Barnett Shale-Gas Play

Play: *Barnett shale*

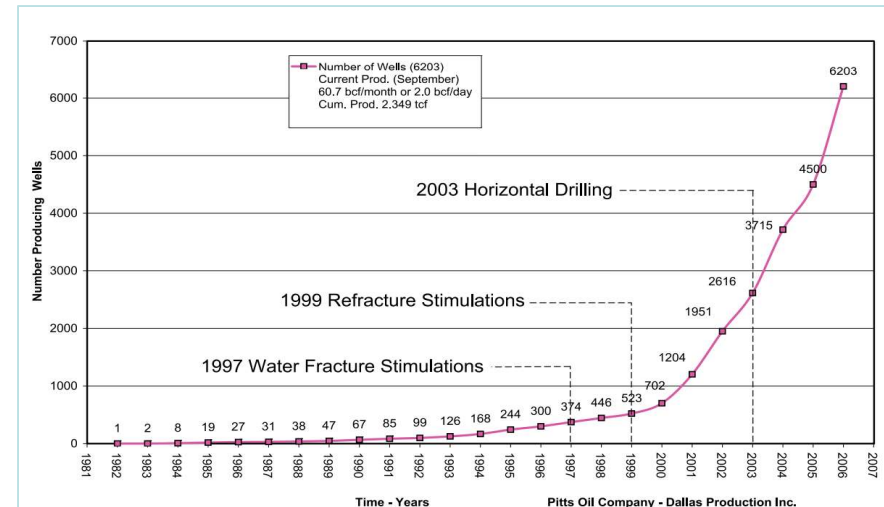
Location: *Northwest of Dallas*

Field: *Newark East*



Field History

- Founded by MEC in 1981, bought out by Devon in 2002
- Original target was the Viola and Ellenburger formation
- Newark East field: Started in Wise county, expansion into Denton
- 2006: Largest field in Texas, 3rd in the nation.
- Technology advances improved field performance.

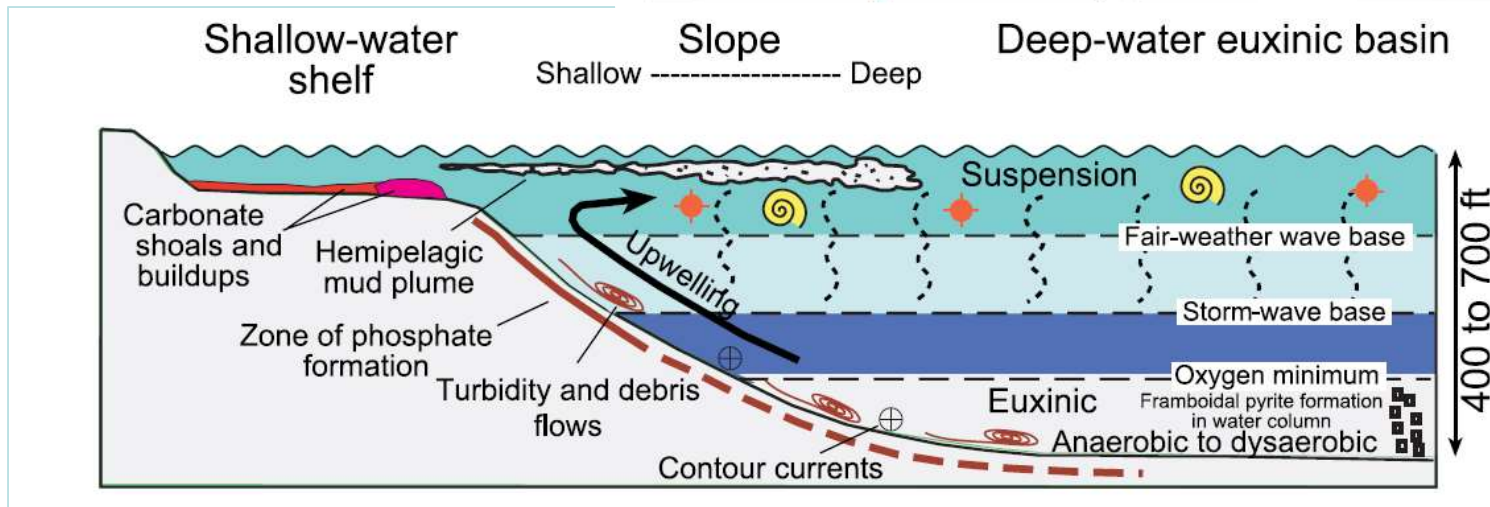
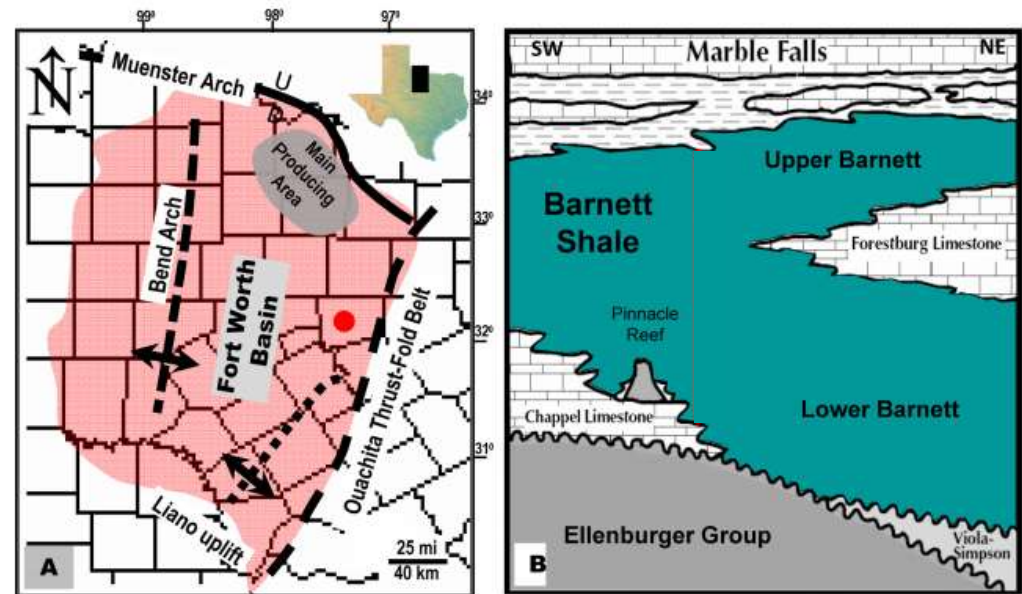


Barnett Shale	
Geologic Age	Late Mississippian
Area size, mile square	5,400(4,065 active)
Depth, ft	6,500-8,500
Thickness, ft	100-600
TOC, %	4-5
Thermal Maturity, Ro%	1.3-2.1
Porosity, %	4-8
Well Avg. IP, MMcfd	2.5
Horizontal lateral, ft	3,950-4,350
TRR, Tcf	43
EUR/Well, Bcf	1.6
Pressure Gradient, psi/ft	0.43-0.45
Well Spacing, AC	116
First Production	1981



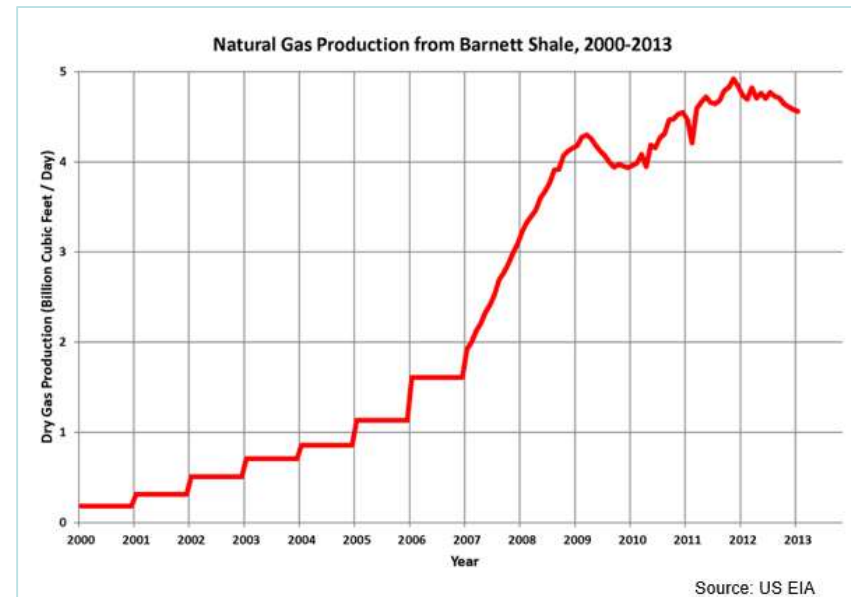
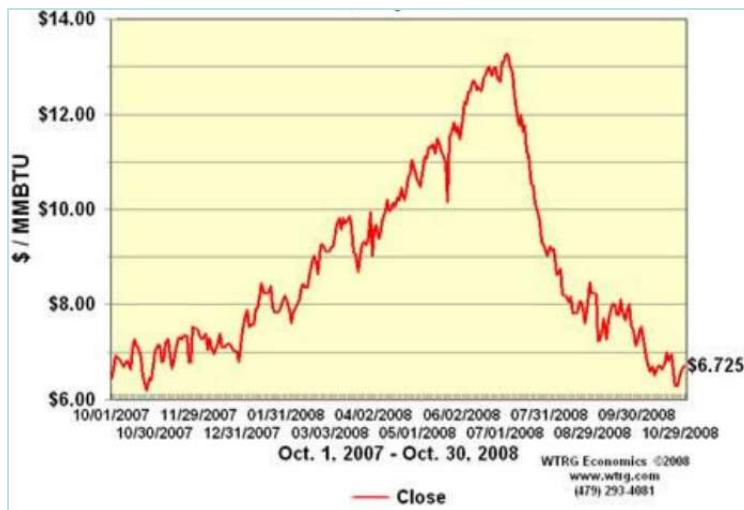
Depositional Setting

- Mississippian age
- Fort Worth Basin
- Deposition: 25 M.Y
- Shale gas system
- Debris transported from shelf region
- Lithofacies: clay to silt

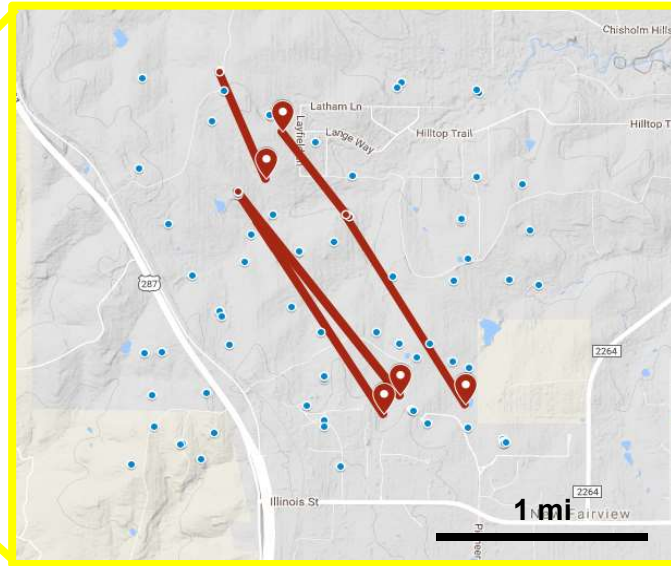
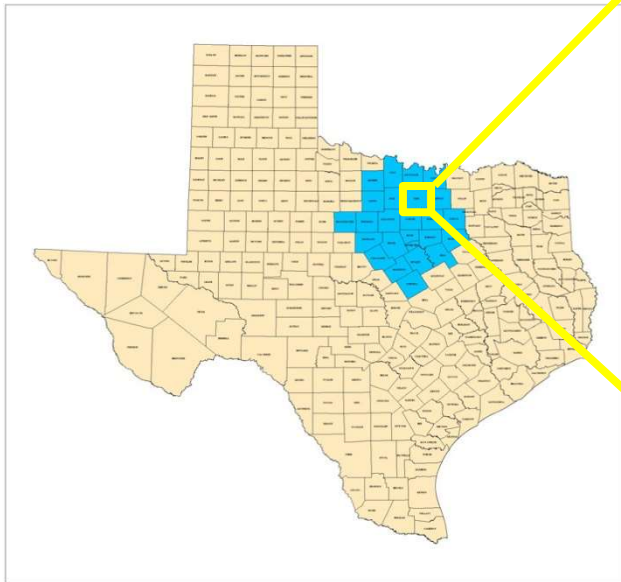


Economics

- Higher gas price and horizontal drilling
- Contributes 8% of natural gas to U.S
- Total production estimated at 4TCF in 2008
- Updated estimated 39 TCF



Study Area

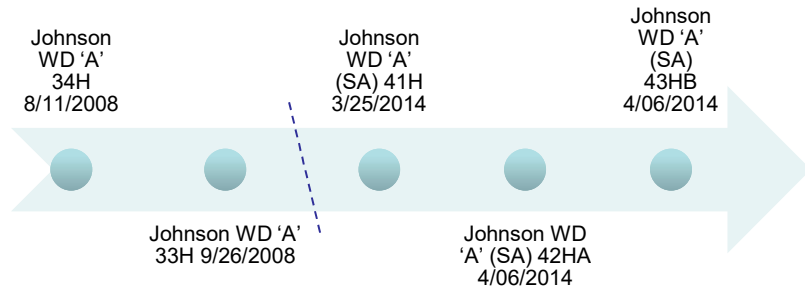
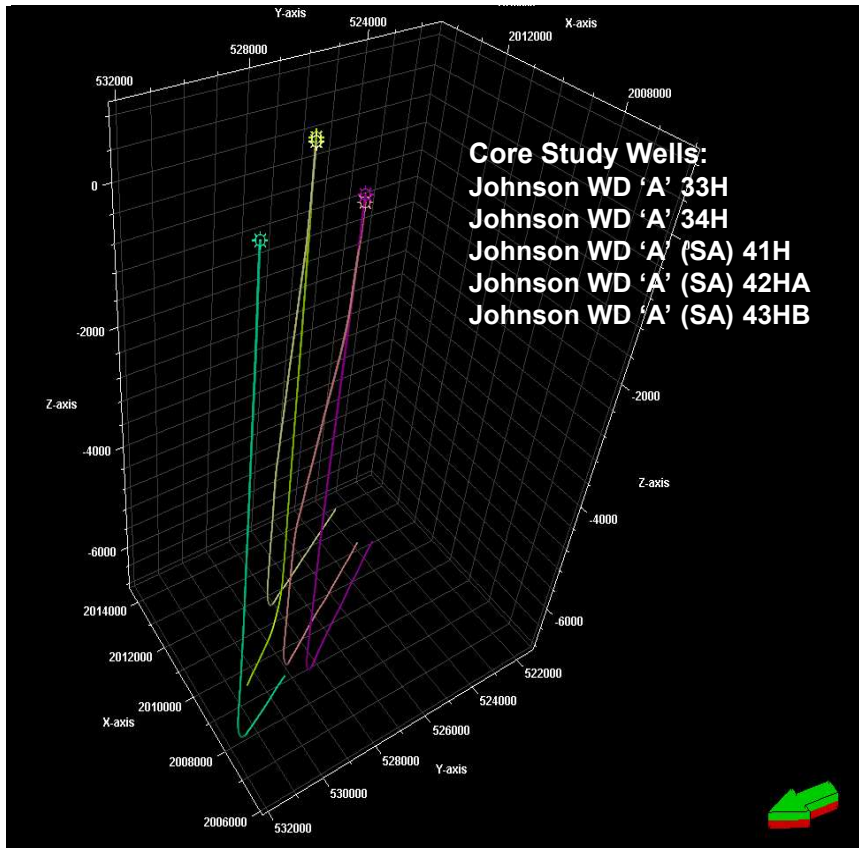


Devon Energy's M14 Asset Area:

- Located in Wise County, Texas
- 81 deviated and horizontal wells
 - Focus group of 5 core wells
- Targets reserves in the Newark East Gas Field



Study Area



	Date Completed	I.P. (MSCFD)	Gp (MMSCF)	Wp (MSTB)
33H	9/26/2008	2007	1298	29.59
34H	8/11/2008	1691	1207	22.57
41H	4/22/2014	755	581	7.47
42HA	5/12/2014	3609	1216	33.87
43HB	5/12/2014	3635	1188	25.10

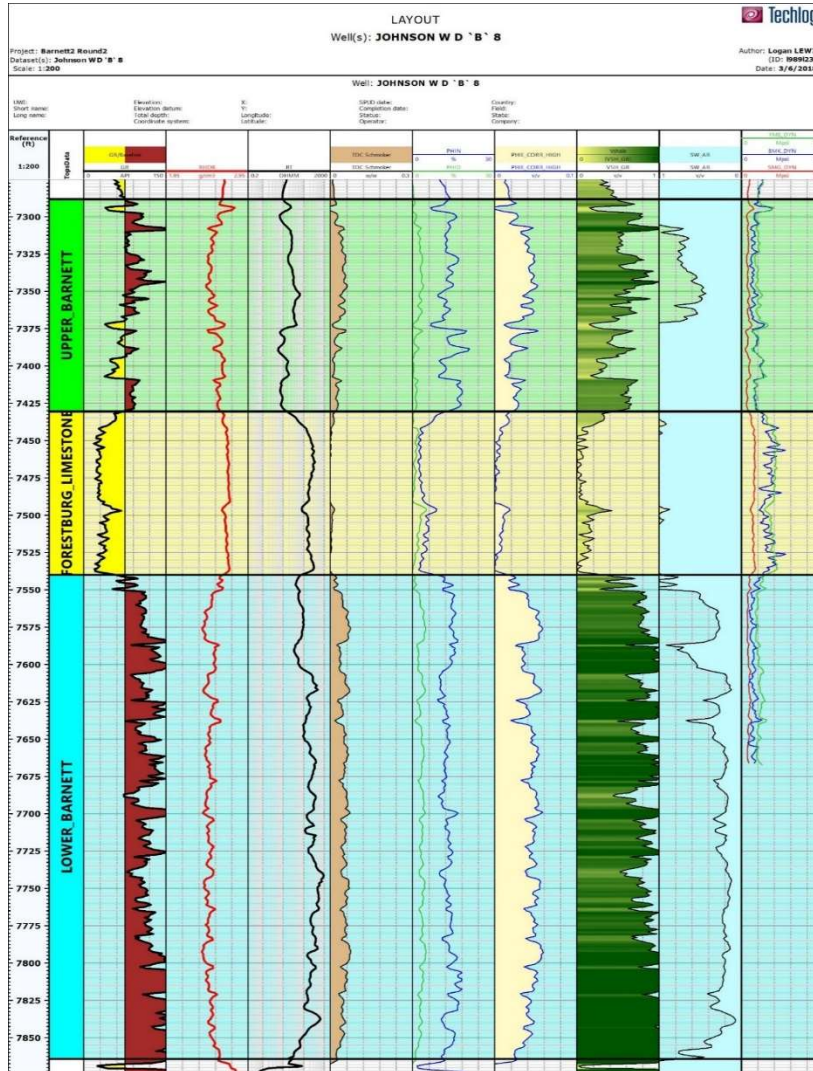




Rock Quality/Petrophysical Evaluation



Petrophysical Evaluation



Shale Volume:

$$V_{SH,GR} = \frac{\gamma_{matrix} - \gamma_{log}}{\gamma_{matrix} - \gamma_{shale}}$$

$$\gamma_{matrix} = 23 \text{ API}$$

$$\gamma_{shale} = 130 \text{ API}$$

Total Organic Content ⁽¹⁾:

$$TOC = (A/\rho_b) - B$$

$$A = 154.497$$

$$B = 57.261$$

Porosity ⁽²⁾:

$$\phi = \frac{\rho_b - \rho_{ma} + TOC(\rho_{ma} - \rho_{TOC})}{\rho_g(1 - S_w) + \rho_w S_w - \rho_{ma}}$$

$$\rho_{ma} = 2.71 \text{ g/cc}$$

$$\rho_{fluid} = 1.0 \text{ g/cc}$$

$$\rho_{TOC} = 1.4 \text{ g/cc}$$

$$\rho_g = 0.3 \text{ g/cc}$$

Water Saturation ^(3,4):

$$S_w^n = \frac{R_w}{\phi^m \times R_t}$$

$$R_w = 0.03 \Omega m \text{ ⁽³⁾}$$

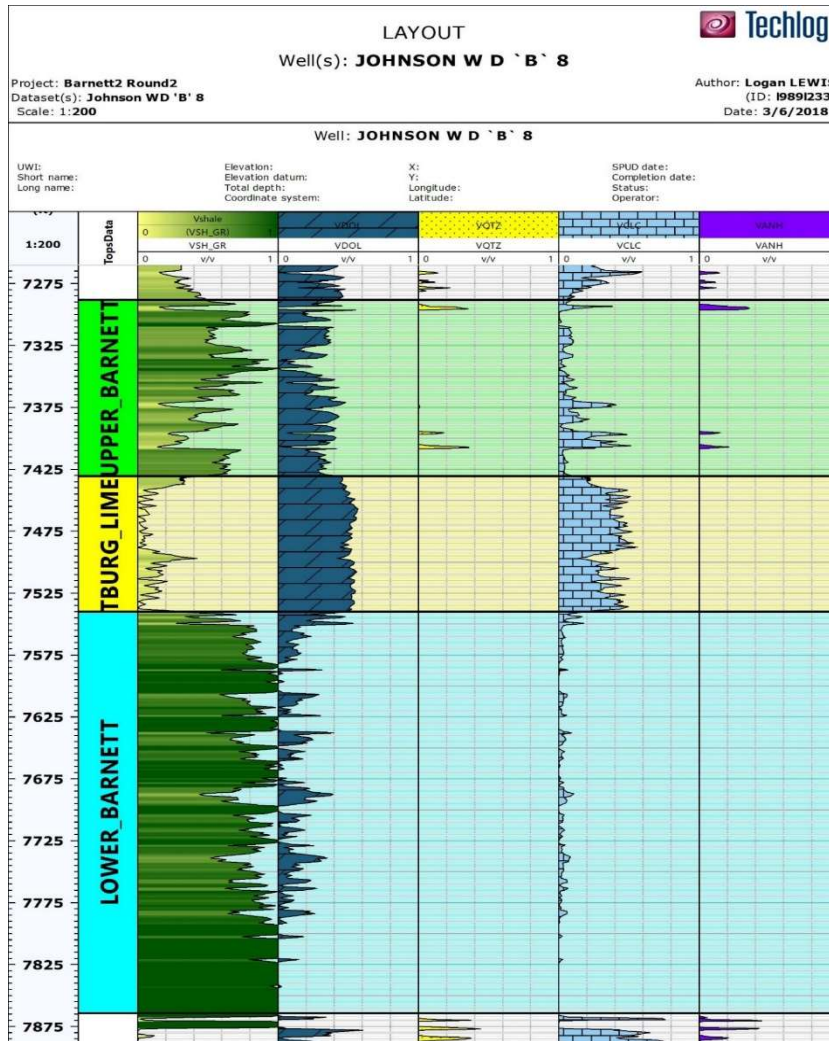
$$n = 2$$

$$m = 1.9$$

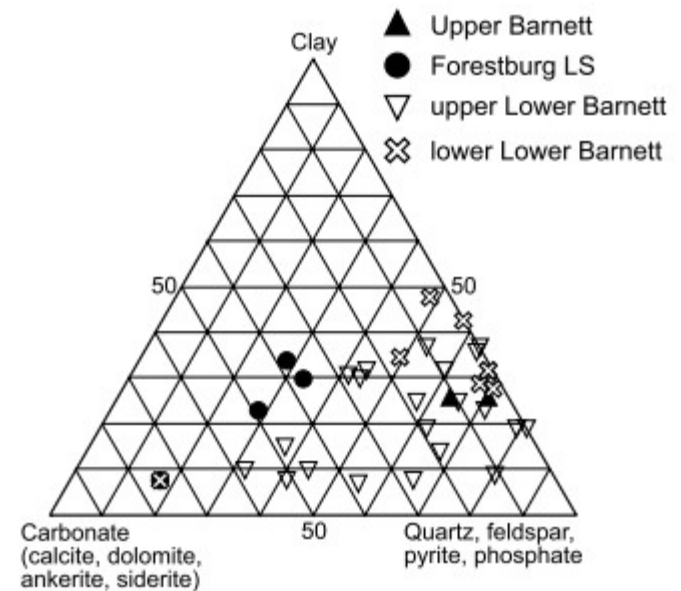
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- (1) Schmoker, 1983
- (2) Sonergeld *et. al*, 2010 (modified by Lewis, 2018)
- (3) Archie, 1941
- (4) Zhang, 2016

Rock Quality Evaluation



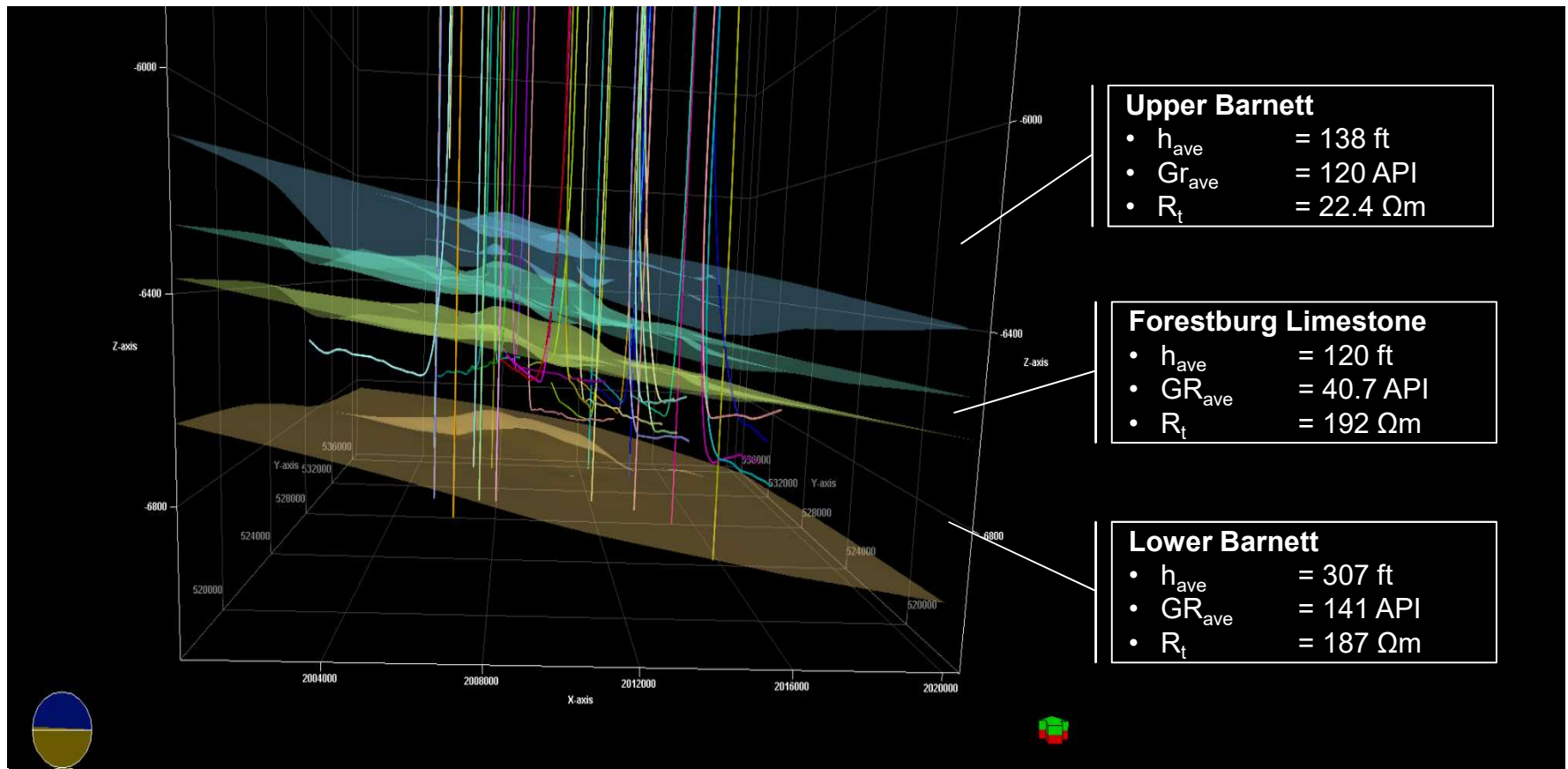
Multi-Mineral Lithology Analysis:



(5) Locks and Ruppel, 2007



Geological Model





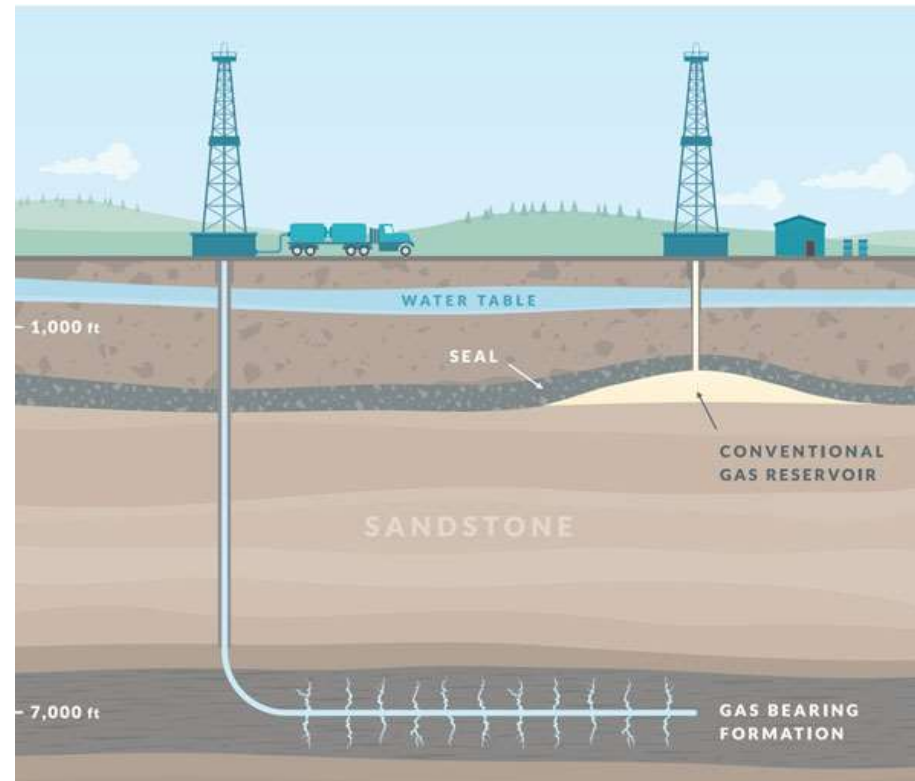
Completion Quality Evaluation



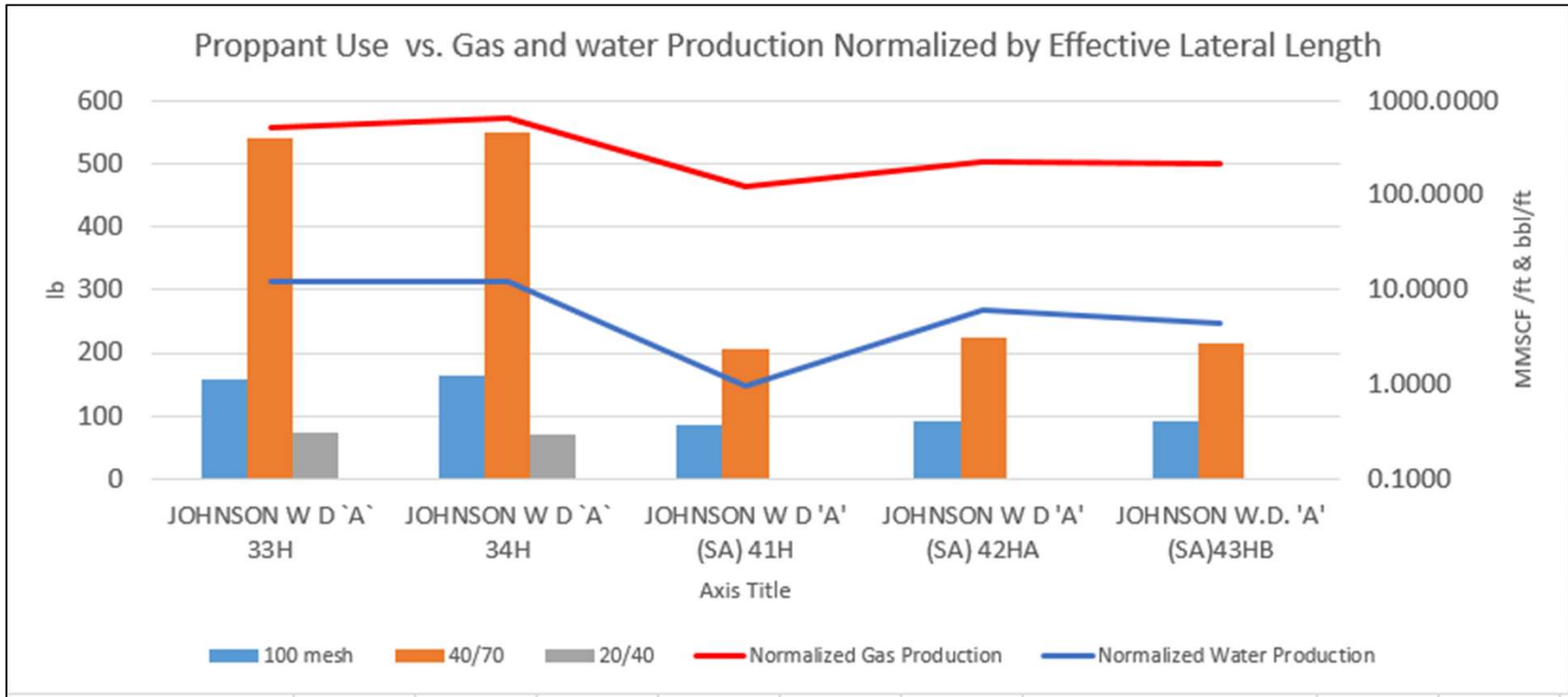
Hydraulic Fracture Design

- The purpose of doing a hydraulic fracture in a shale formation is to widen the pore space in order for hydrocarbons to mobilize.

--Montgomery et al., 2005



Hard Data

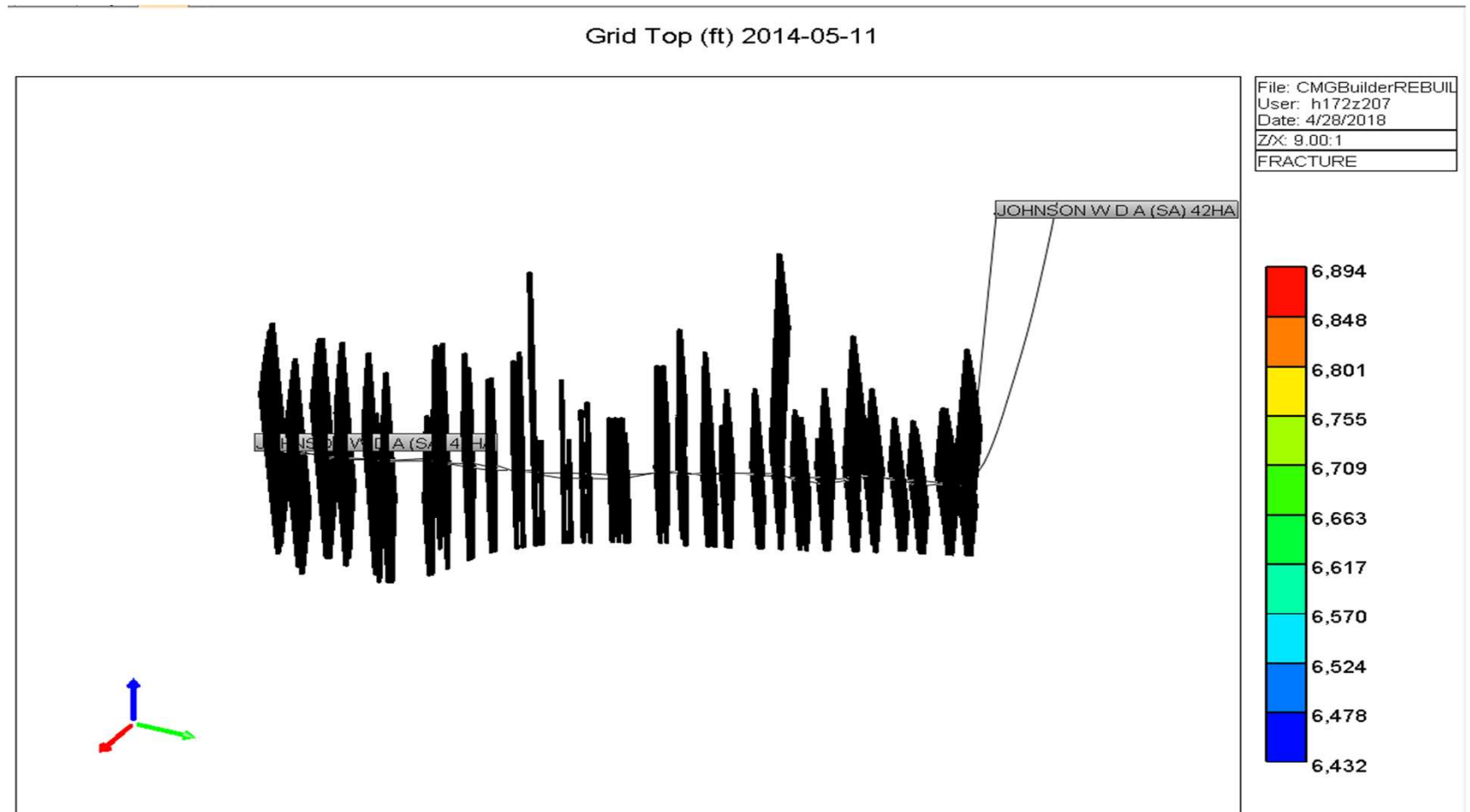


- **41H 42HA 43HB are only using 100 mesh and 40/70**

NAME	Effective Lateral Length
JOHNSON W D `A` 33H	2474
JOHNSON W D `A` 34H	1883
JOHNSON W D `A` (SA) 41H	4799
JOHNSON W D `A` (SA) 42HA	5445
JOHNSON W.D. `A` (SA)43HB	5656



Simulated Frac Model





Field Evaluation



P_{50} Well Determination

- P_{50} is targeted because it is close to the mean value of the data.
- Knowing the P_{50} well allows for the best average value to be used as a reference as to what is to be expected.



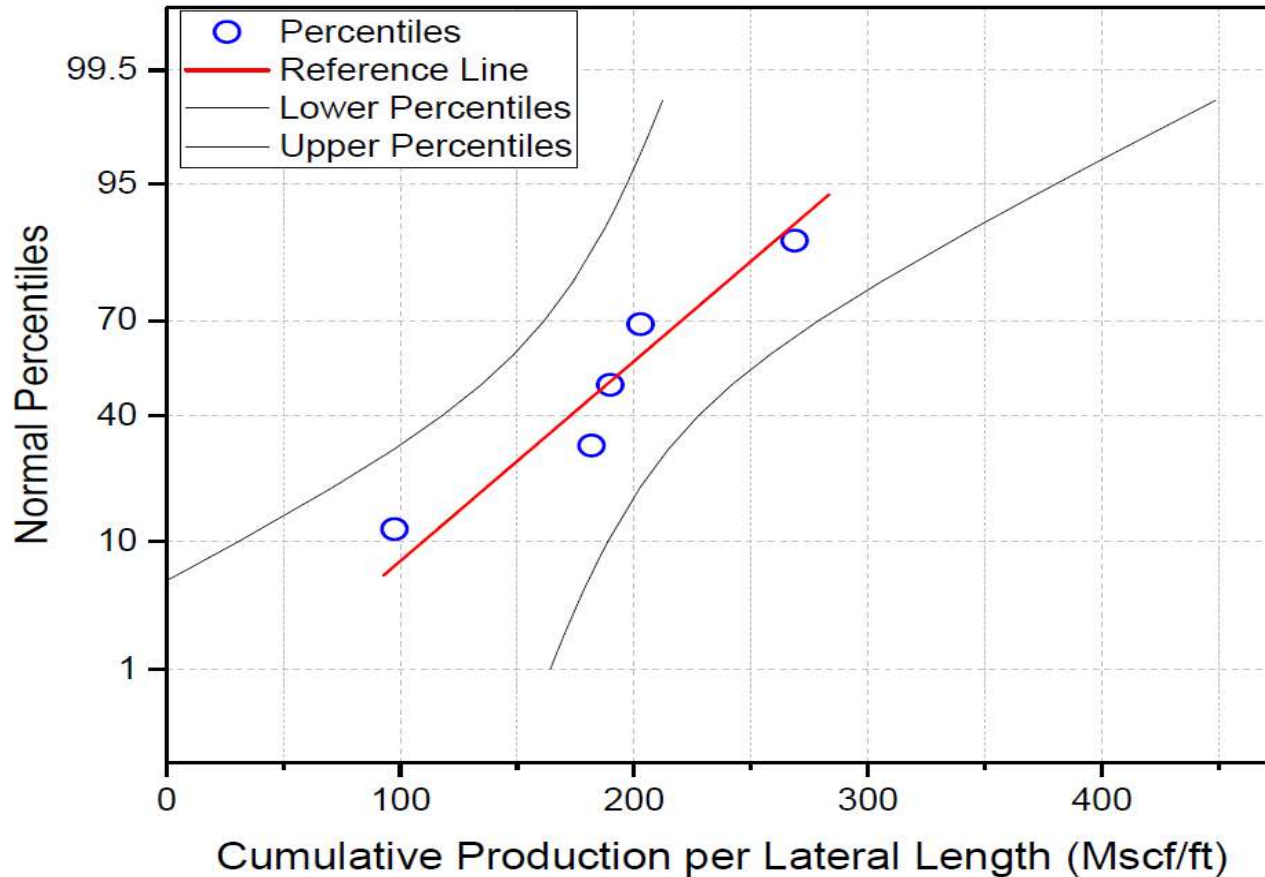
Process

- The production indicator chosen was 800 days of cumulative gas.
- Normalized production data.
- Identified P_{50} well based on cumulative production, linear flow, and proppant data.

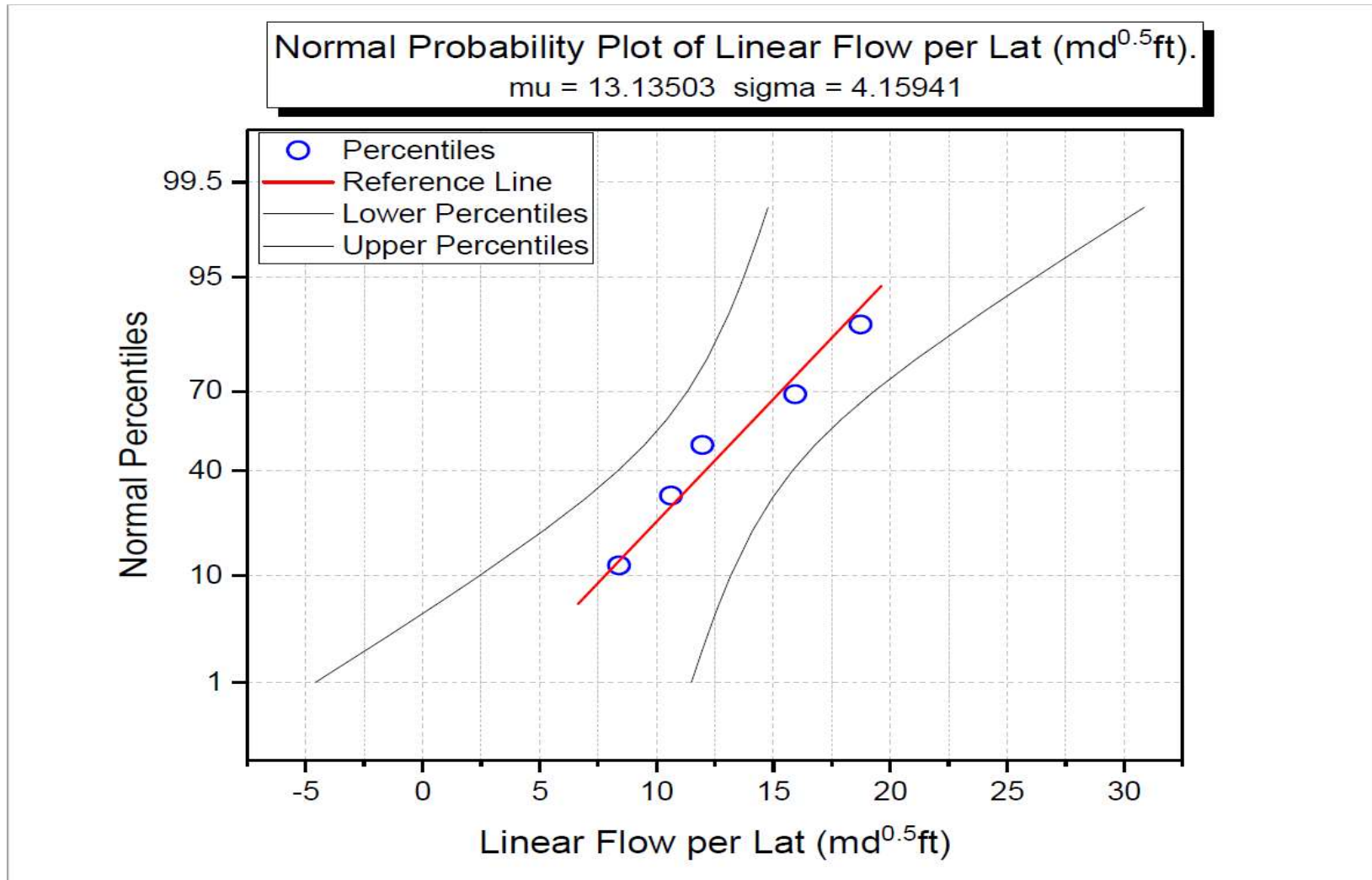


P₅₀ Cum. Production/Lat. Length

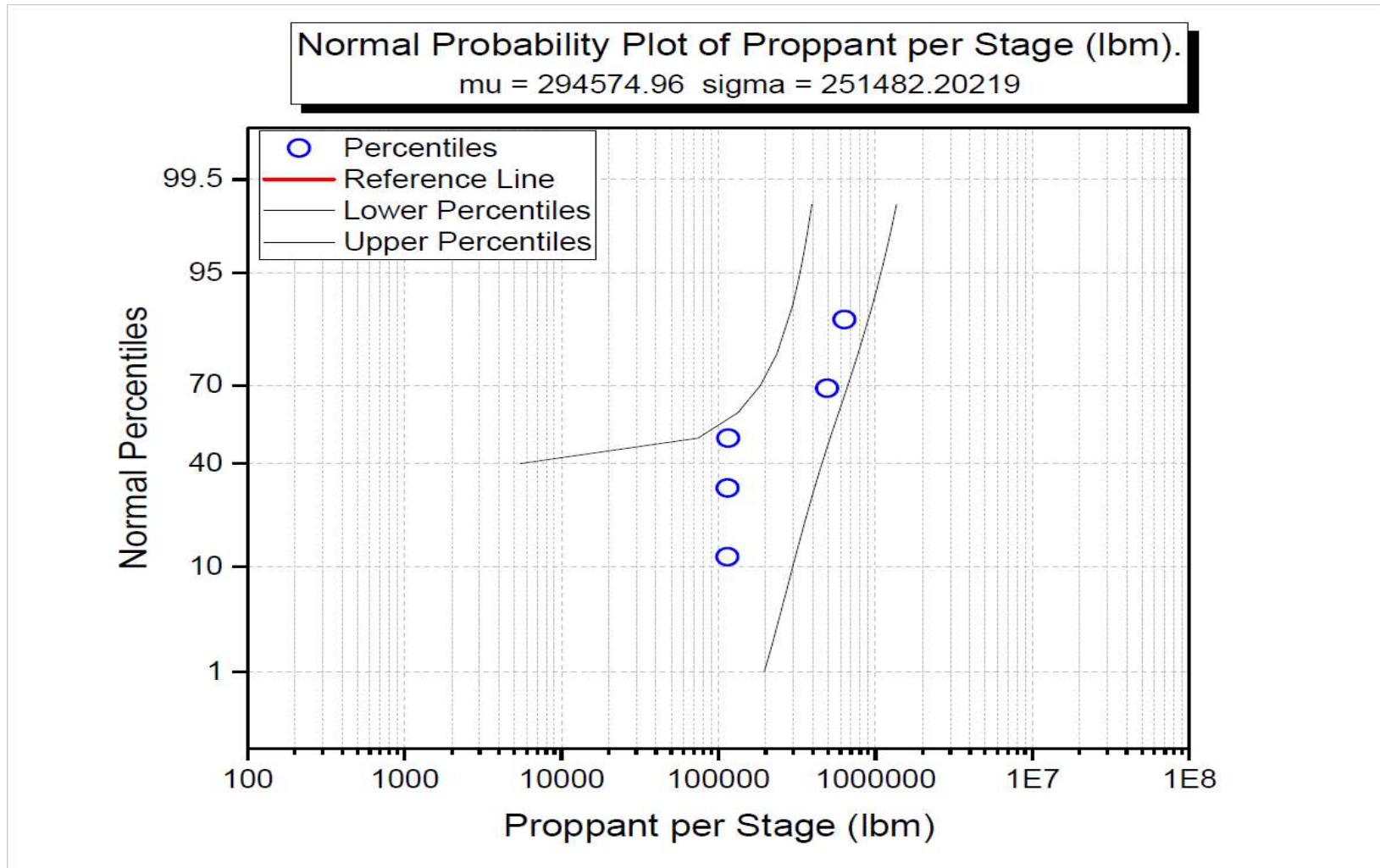
Normal Probability Plot of Cumulative Production per Lateral Length (Mscf/ft).
mu = 188.13029 sigma = 61.15086



P₅₀ Linear Flow/Lat. Length

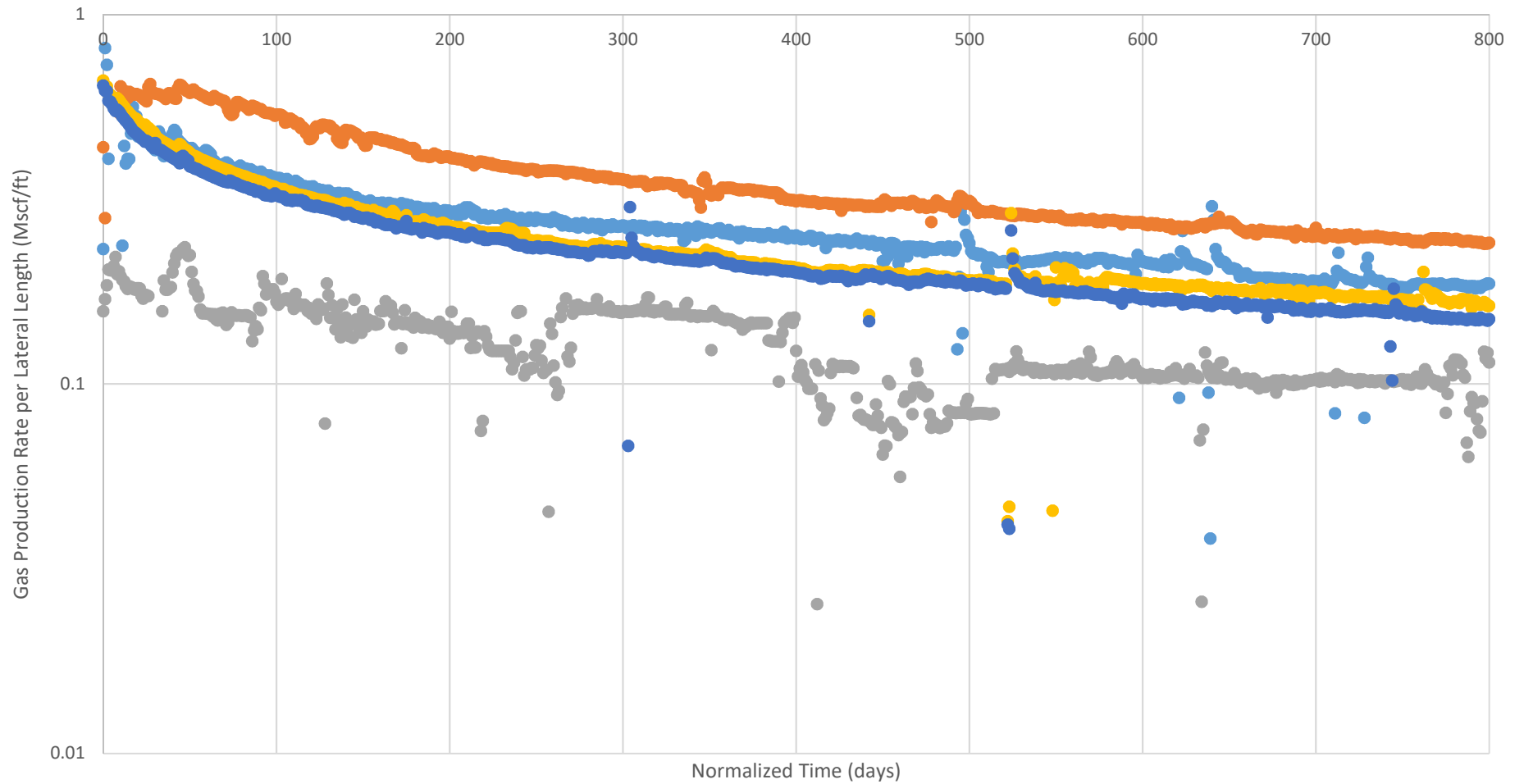


P₅₀ Proppant/Stage

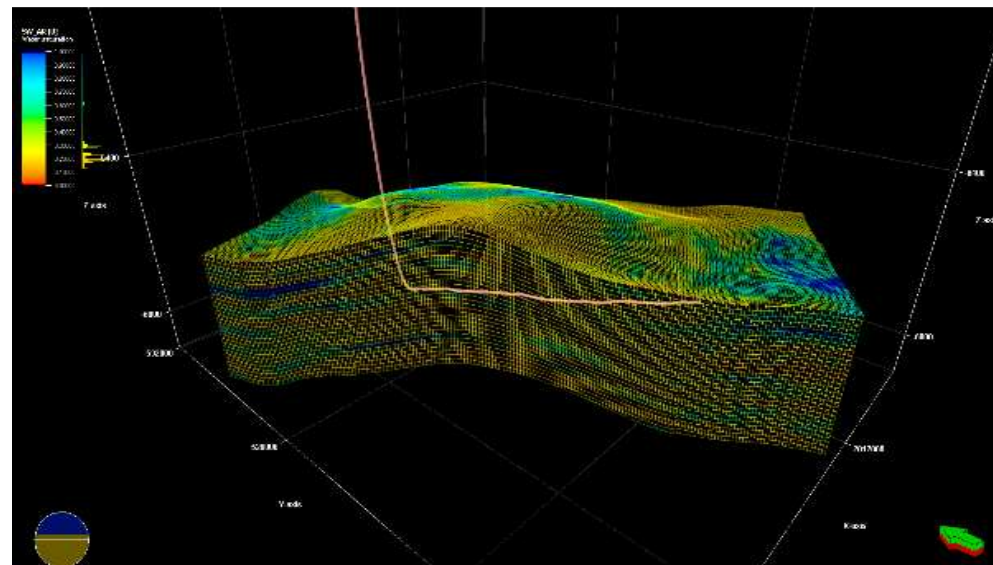


P_{50} (800 Days)

P_{50} Estimation (0-800 days)



Chosen P_{50} Well

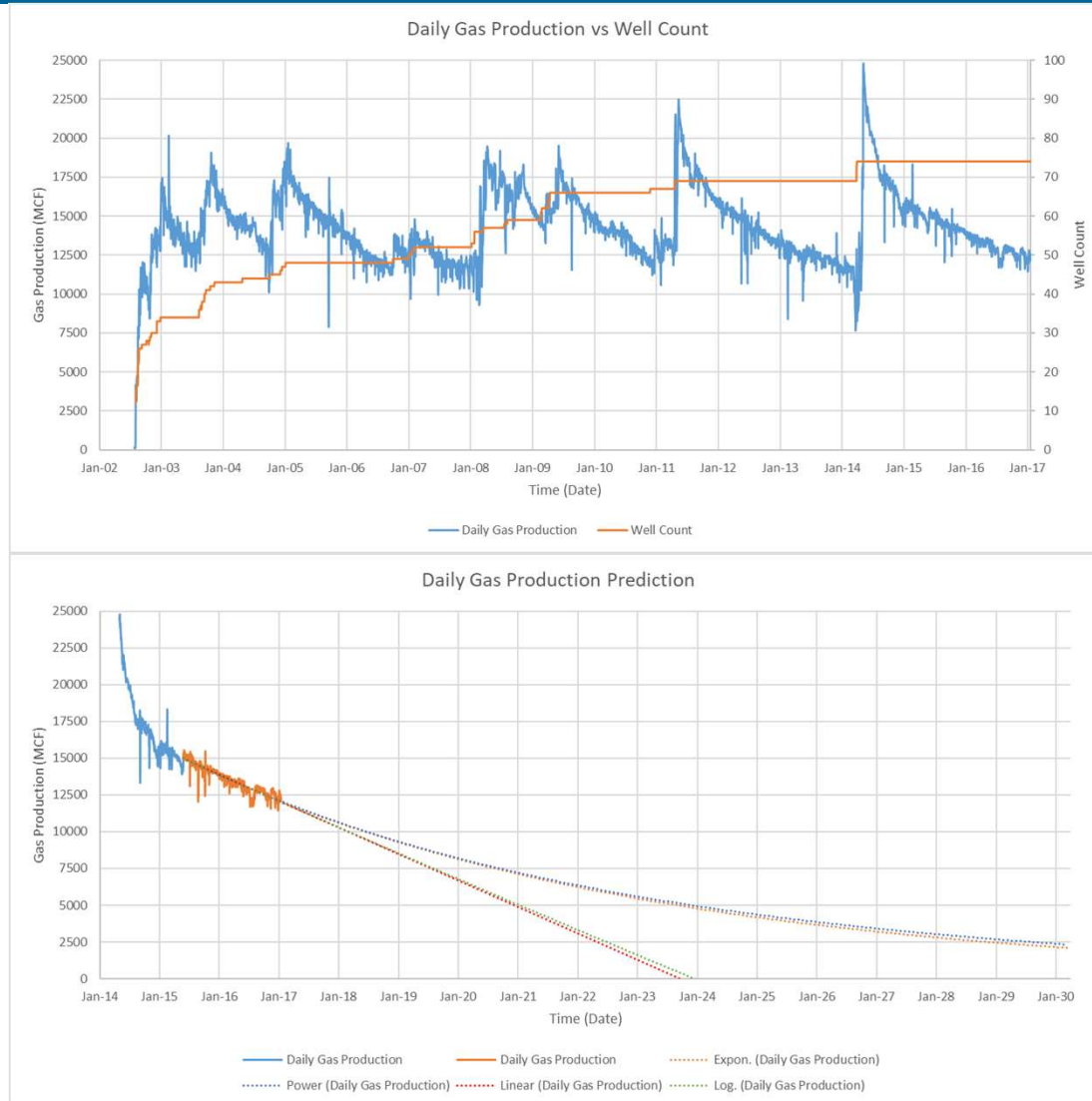




Operation Quality Evaluation

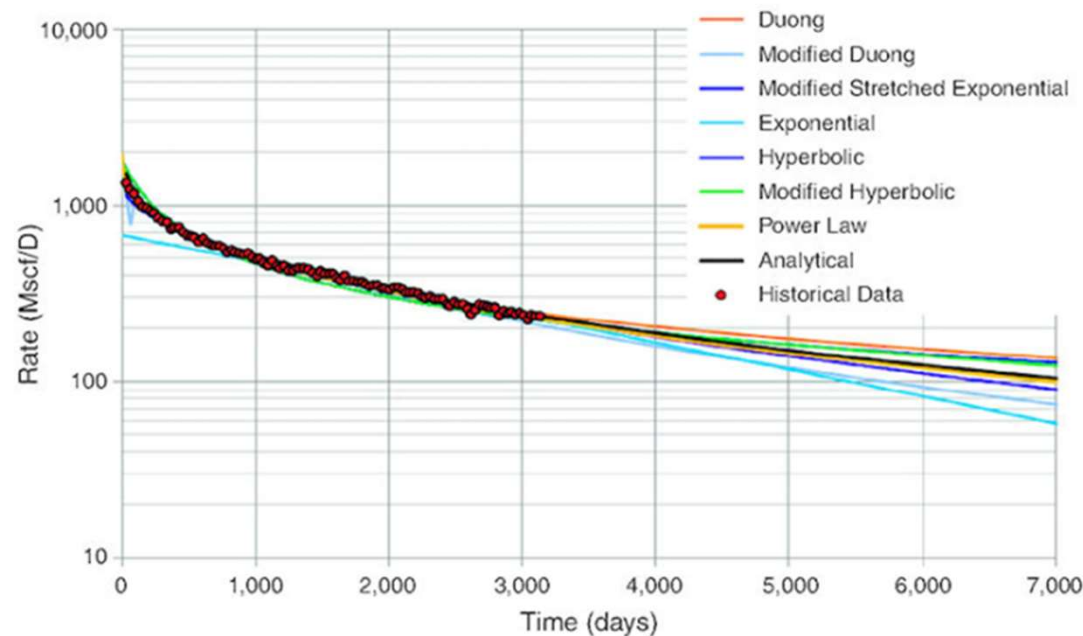


Field Production Data



Decline Curve Analysis

- **Methodology:** Multiple decline curves were applied to the 5 target wells and field as a whole in IHS Harmony. The goal was to determine the representative trends that projects the well's economic life and forecast future cumulative production.



Decline Curve Analysis

- **Parameters:**
 - Devon Energy has a set cutoff rate of 20 Mscf/day for gas wells
 - By using DCA, it is predicted that gas production will fall to 900Bscf/yr by 2030 from the peak of about 2Tscf/yr
 - From this DCA forecast, it is likely the Barnett field as a whole will no longer be a major contributor to natural gas production in the year 2030
- **Reasons for production decline of Barnett shale gas wells**
 - Due to a shrinkage of viable space and the decrease of sweet spots, future drilling in the Barnett has been waning
 - Production analysis has found that older wells tend to have better decline performance than new wells
 - Likely due to poorer reservoir rock quality and well interface (well spacing and drainage area)



Decline Curve Analysis

- **Curves Considered:**
 - Arps Equations – Exponential, Harmonic, Hyperbolic
 - Power-Law Exponential Method
 - Duong Method
 - Stretched-Exponential Production Decline
 - Known to be conservative prediction for decline models in tight formations
- **Best Fits:**
 - Stretched Exponential “Best Fit Whole”
 - Matched 5/5 target wells within P 50 range
 - Underestimates EUR
 - Stretched Exponential – with calculated values
 - Matched 4/5 target wells within P50 range
 - Overestimates EUR



Decline Curve Analysis

– Stretched Exponential

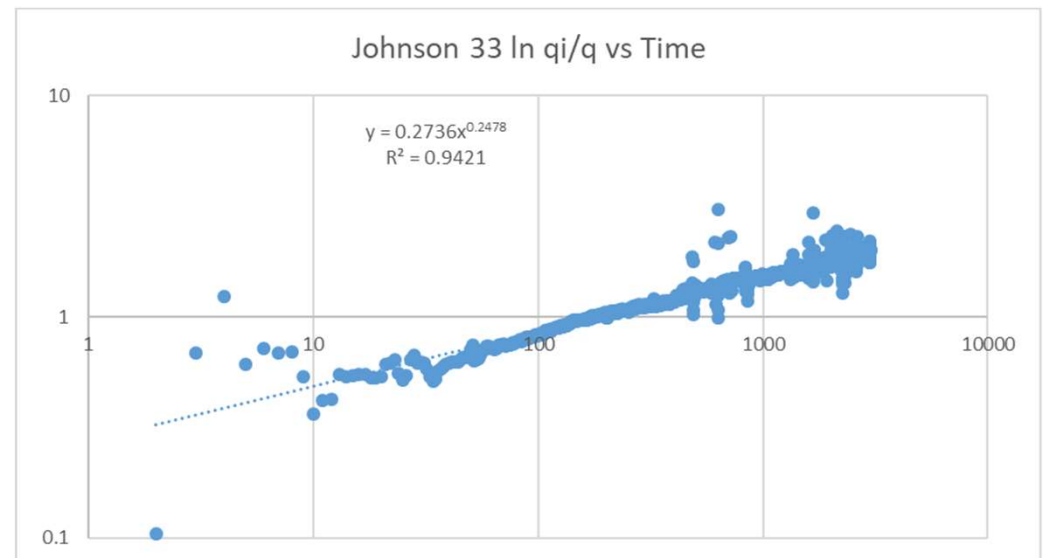
- Calculated from Observed behaviors of $q(t)$

- $q(t) = q_1 e^{-\left(\frac{t}{\tau}\right)^n}$

- n is found and τ is calculated

- $\tau = e^{\frac{-\ln \text{intersect}}{n}}$

- $\tau = \left(\frac{n}{D_i}\right)^{\frac{1}{n}}$



Decline Curve Analysis

Company: Barnett 2
 On Stream: 05/12/2014
 Status Date: 04/06/2014
 Current Status: Flowing

JOHNSON W D 'A' (SA) 42HA

Gp: 1216 MMscf
 Np: 0.000 Mstb
 Wp: 33.107 Mstb
 DTD(MD): 13556.0 ft(KB)



Curve Fit	EUR (MMSCF)	Qf (MSCFD)
Stretched Best Fit Whole	9629.0	10845.4
Stretched Calculated Values	5605.5	6821.9



Decline Curve Analysis

Conclusions:

- Duong's method is generally accurate for Barnett unconventional wells, especially in early production
- Stretched exponential produces similar results
- Hyperbolic and Harmonic decline (and $b > 1$) are useful in modelling early flow regimes
- The stretched exponential model with calculated and best fit whole curves yielded realistic forecasts that agreed with RTA and the probabilistic analyses



RTA

Data

- Production Rates
- Langmuir Curves
- Pressure Data
 - Tubing
 - Casing
- Reservoir Data
 - Initial Pressure
 - Temperature
- Completion Design
 - Stages
 - Clusters

Analysis

- Log-log rate vs. time
 - Flow regime
- Analytical Model:
 - Type curve
 - FMB
 - History matching
- Probabilistic Analysis:
 - Altered-case scenarios and their likelihood

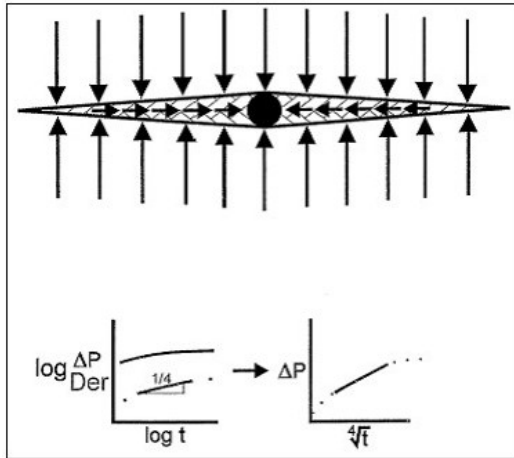
Results

- Reservoir Parameters:
 - OGIP
 - EUR
 - Permeability
 - A_{SRV}
 - Geomechanical influence
- Fracture Parameters:
 - X_f
 - F_{CD}
 - X_l



Background and Theory

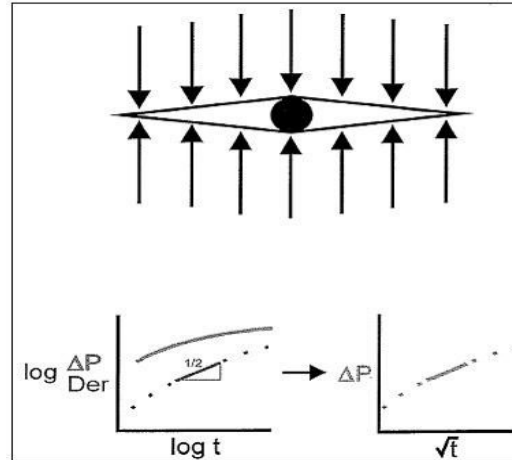
Flow Regimes of Interest:



Bilinear Flow:

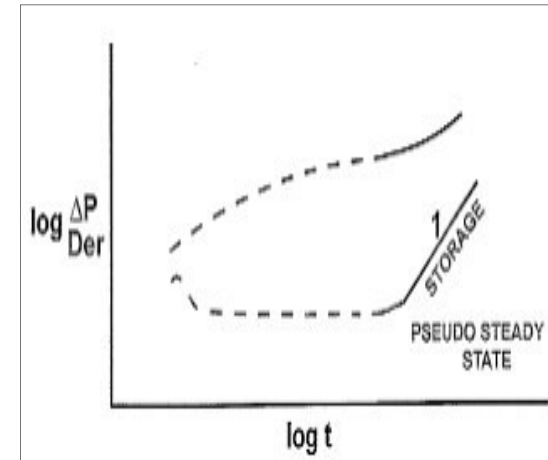
- $1/4$ slope
- Early flow
- Fracture drainage

* Can occur prevalently in naturally fractured systems or when $x_f > h_f$



Linear Flow:

- $1/2$ slope
- Majority of flow
- Occurs after fractures have stabilized



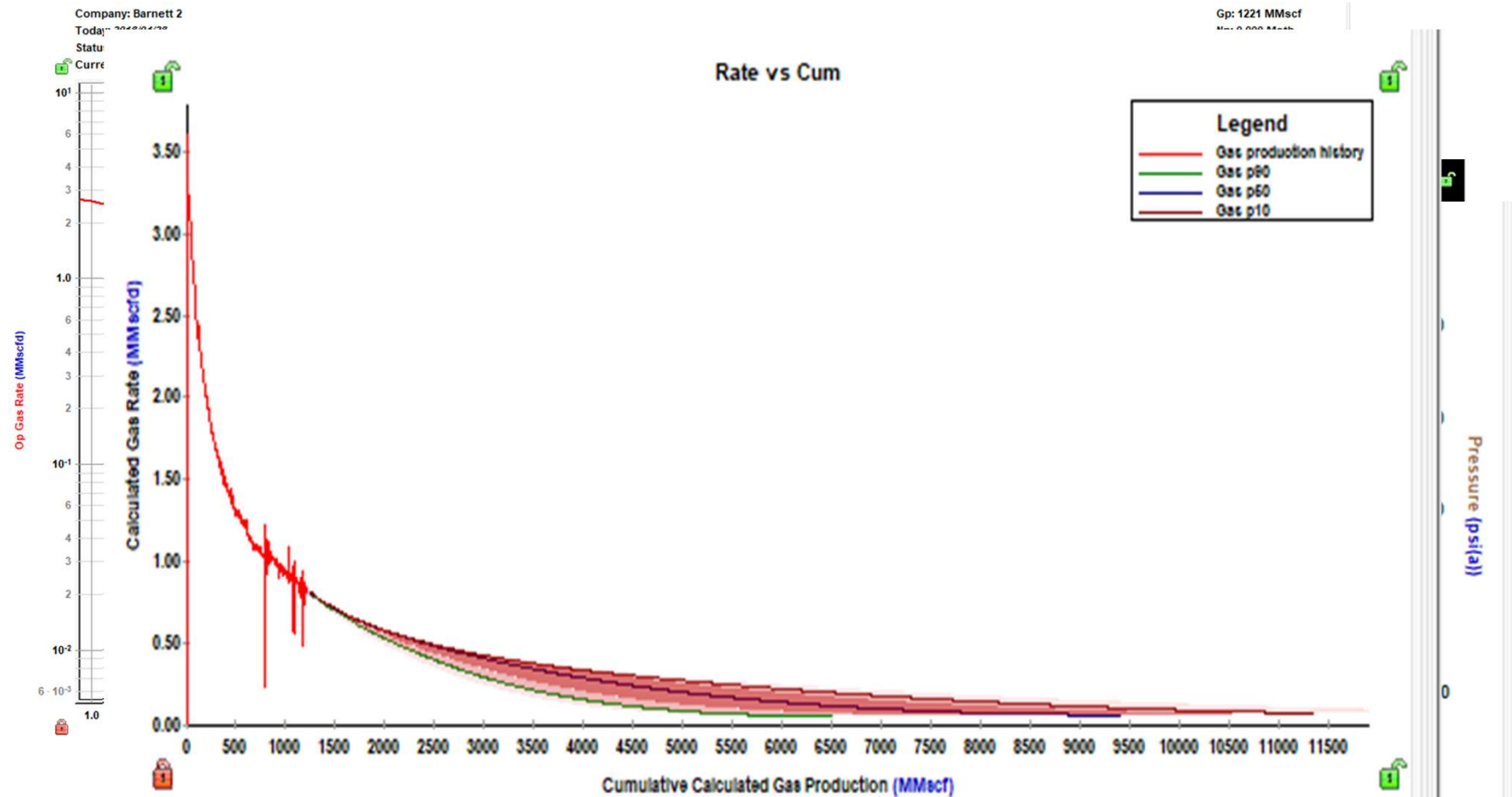
Boundary Dominated Flow:

- Unit slope
- Late flow
- Reservoir boundaries have been realized

(1) Fekete.com



RTA: Johnson WD 'A' (SA) 42H

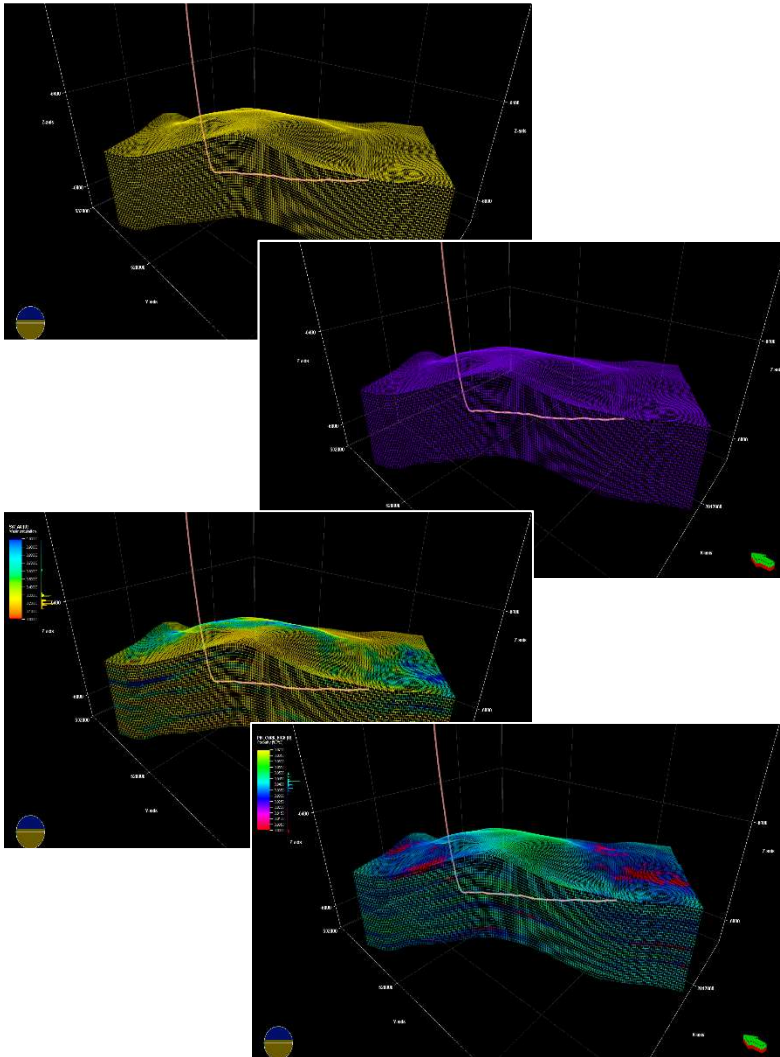




Well Spacing Optimization



Base Model



Base Properties:

P_i (psia)	3500.0
k_m (nD)	350.0
S_w (%)	30.1
Φ (%)	4.0
F_{CD}	Gohfer
$X_{f,1/2}$ (ft)	Gohfer





Economic Viability



Acknowledgements

- We would like to thank Dr. Amirmasoud Kalantari Dahaghi
- Devon Energy for the provided data
- Schlumberger, IHS Harmony, Gohfer, CMG for providing academic licenses

Thank you!



References

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3. G. Archie, "The Electrical Resistivity Log as an Aid in Determining Some Reservoir Characteristics," Society of Petroleum Engineers, Dallas, TX, 1941.
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Questions? Photoelectric Logging

- Measures the average atomic number of the elements in formation as the Photoelectric Effect (PE). Known PE values for common lithologies are generally very accurate.
- Usually combined with density for a Litho-density Log
- Photoelectric absorption coefficient (U) and photoelectric absorption of matrix rock (U_{MA}) can be calculated:

$$U = PE * RHOB$$

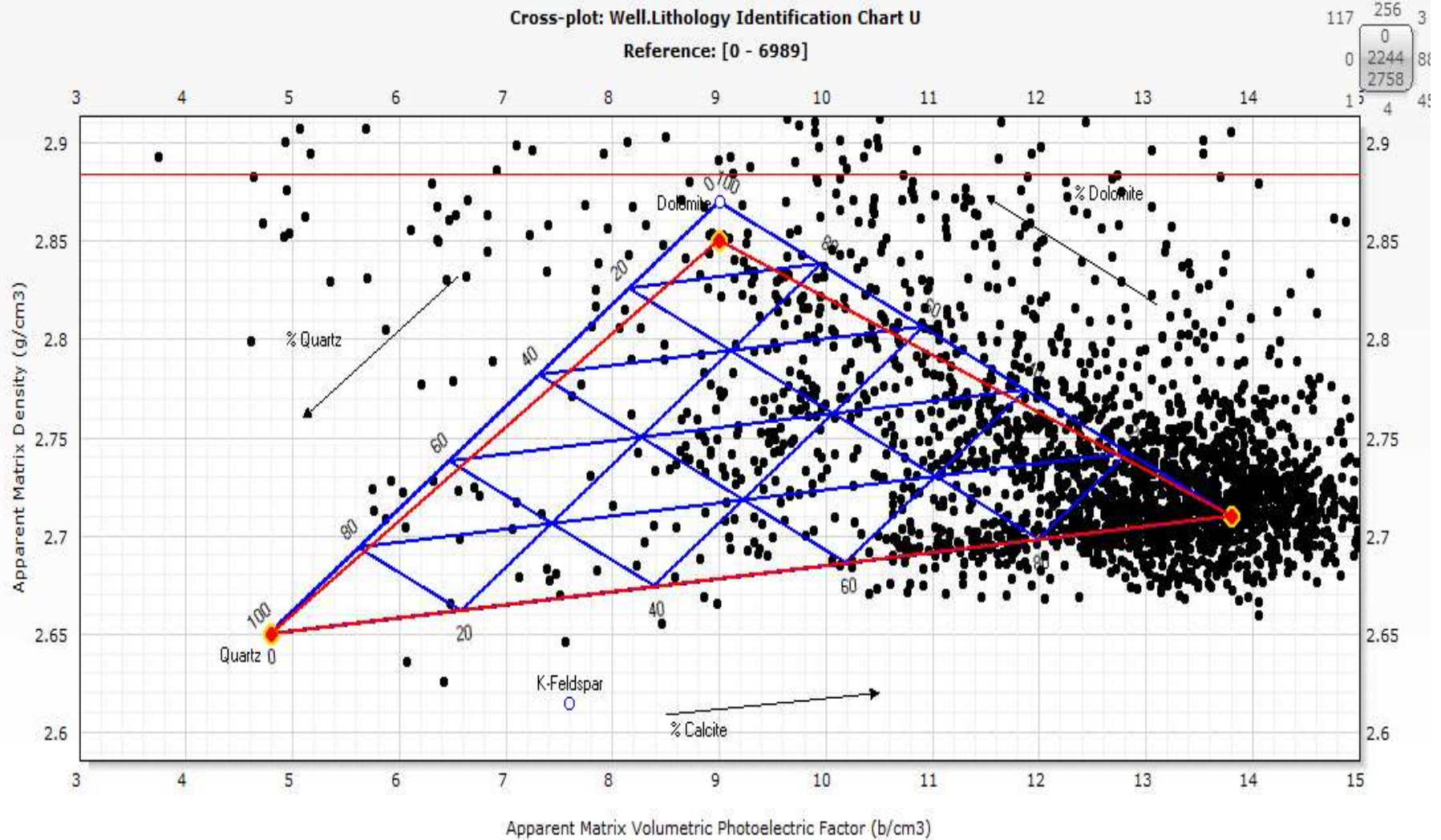
$$U = U_{MA} (1 - PHIE - VSH)$$

- This U_{MA} can be plotted versus the apparent matrix density of known lithology types.

Source: Crain's Petrophysical Handbook (<https://www.spec2000.net/13-lithpdn.htm>)



Questions? Photoelectric Logging



Johnson WD 'A' (SA) 41H

Company: Barnett 2
 On Stream: 04/22/2014
 Status Date: 03/25/2014
 Current Status: Flowing

Gp: 581 MMscf
 Np: 0.000 Mstb
 Wp: 7.472 Mstb
 Qcond: 0.000 Mstb

JOHNSON WD 'A' (SA) 41H

